

TITLE OF THE INVENTION

SERVO CONTROLLER

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention relates to a servo controller for driving a load machine, such as a feed shaft for use with a machining tool or an arm for use with an industrial robot, by using a motor. More particularly, it relates to a servo
10 controller for performing path control on a machine having two or more axes.

Description of Related Art

There have been provided prior art servo controllers for carrying out feed forward control so as to compensate for a
15 delay in response to an instructed value of an amount to be controlled such as the position or speed of a target machine. For example, Japanese patent publication No. 2762364 (reference 1) discloses a servo controller for differentiating a position instruction signal so as to obtain an amount of feed
20 forward control associated with the position of a target machine, for adding the amount of feed forward control to an amount of control acquired by carrying out position loop control so as to obtain a speed instruction signal, for adding an amount of feed forward control associated with the speed
25 of the target machine, which is obtained by differentiating the amount of feed forward control associated with the position of the target machine, to a value acquired by carrying out speed loop control so as to obtain an electric current instruction signal, and for performing servo control, thereby improving
30 the response of position control (see Fig. 1 of Japanese patent

publication No. 2762364, for example).

Japanese patent application publication (TOKKAI) No. 2000-92882 (reference 2) discloses a servo controller in which a simulated control circuit is so constructed as to control
5 a mechanical system model which is approximated as a two-inertia oscillation system and is provided with a torque transmission mechanism, a load machine, and an electric motor, and to add the position, speed, and torque of a simulated electric motor of the simulated control circuit to a value
10 acquired, as an amount of feed forward control, by carrying out position loop control and speed loop control, thereby improving the response of position control without exciting vibrations even when the stiffness of the target to be controlled is low and the target to be controlled has resonance
15 characteristics (see Fig. 25 of Japanese patent application publication (TOKKAI) No. 2000-92882, for example).

A problem with the prior art servo controller disclosed in Japanese patent publication No. 2762364 is that while the prior art servo controller can offer adequate performance when
20 the stiffness of the target to be controlled is high and the target to be controlled can be assumed to be a rigid body, mechanical resonance vibrations can cause vibrations in the position and speed of the target to be controlled, which are amounts to be controlled, when the prior art servo controller
25 is applied to a target to be controlled having low stiffness and resonance characteristics and the response of position control is increased, the positioning accuracy and path tracking accuracy decrease, as shown in Fig. 13.

A problem with the other prior art servo controller
30 disclosed in Japanese patent application publication (TOKKAI)

No. 2000-92882 is that when the target to be controlled can be assumed to be a two-inertia oscillation system, while the position of the target to be controlled completely responds to the position of the simulated control circuit at all times and therefore the response of the position control can be improved without exciting vibrations, the simulated control circuit constitutes a feedback control system and therefore the impulse response is not made to become symmetric. As a result, the response path of the target to be controlled does not become symmetric even if a symmetric path is provided as the instructed path, and therefore, when the target to be controlled is instructed to travel between two positions along the same instructed path so that the direction of travel is changed as shown in Fig. 14, a difference can occur between the two response paths of the round trip. This results in the generation of scratches on a machined surface of a mold when the mold is machined with reciprocating machining.

SUMMARY OF THE INVENTION

The present invention is proposed to solve the above-mentioned problems, and it is therefore an object of the present invention to provide a servo controller that can reduce vibrations that originate from mechanical characteristics, and that can make the two response paths of a round trip of a target to be controlled match each other.

In accordance with the present invention, there is provided a servo controller including a mechanical characteristic compensation unit for attenuating components each having a predetermined frequency and each corresponding to a characteristic of a target machine to be driven, which

are included in a position instruction signal corrected by an FIR filter unit, so as to compute a plurality of feed-forward signals respectively associated with the position, speed and torque of the target machine, and a feedback compensation unit
5 for driving the target machine to be driven according to the plurality of feed-forward signals respectively associated with the position, speed and torque of the target machine.

Because the mechanical characteristic compensation unit thus attenuates components each having a predetermined
10 frequency and each corresponding to a characteristic of the target machine to be driven, which are included in the position instruction signal, so as to compute the plurality of feed-forward signals respectively associated with the position, speed and torque of the target machine, the servo
15 controller can reduce vibrations that originate from the characteristics of the machine. Furthermore, because the mechanical characteristic compensation unit delivers the computed feed-forward signals to the feedback compensation unit, the servo controller makes it possible for the position
20 of the machine to respond completely to the input of the mechanical characteristic compensation unit, i.e., the output of the FIR filter unit. In addition, because the FIR filter unit can easily make the response path with respect to a symmetric instructed path become symmetric, and, when the
25 target machine is made to travel between two positions along the same path, can make the two response paths of the round trip of the target machine match each other, the servo controller can provide machined surfaces having no irregularities even when carrying out reciprocating
30 machining.

Further objects and advantages of the present invention will be apparent from the following description of the preferred embodiments of the invention as illustrated in the accompanying drawings.

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BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a block diagram showing a servo controller in accordance with embodiment 1 of the present invention;

Fig. 2 is a diagram showing a symmetric impulse response;

10 Fig. 3 is a block diagram showing the whole of the servo controller in accordance with embodiment 1 of the present invention;

Fig. 4 is a diagram showing an instructed path that is provided for a target machine to be driven by the servo
15 controller in accordance with embodiment 1 of the present invention, and a response path of the target machine to be driven;

Fig. 5 is a block diagram showing a servo controller in accordance with embodiment 2 of the present invention;

20 Fig. 6A is a diagram showing an instructed path that is provided for a target machine to be driven by the servo controller in accordance with embodiment 2 of the present invention, and a response path of the target machine to be driven;

25 Fig. 6B is a diagram showing an instructed path that is provided for the target machine to be driven by the servo controller according to embodiment 1 and a response path of the target machine to be driven;

Fig. 7 is a block diagram showing a servo controller in
30 accordance with embodiment 3 of the present invention;

Fig. 8 is a diagram showing an example of a gain curve of a fifth-order IIR filter;

Fig. 9A is a diagram showing an instructed path that is provided for a target machine to be driven by the servo controller in accordance with embodiment 3 of the present invention, and a response path of the target machine to be driven;

Fig. 9B is a diagram showing an instructed path that is provided for the target machine to be driven by the servo controller according to embodiment 1 and a response path of the target machine to be driven;

Fig. 10 is a block diagram showing a servo controller in accordance with embodiment 4 of the present invention;

Fig. 11 is a diagram showing an instructed path that is provided for a target machine to be driven by the servo controller in accordance with embodiment 4 of the present invention, and a response path of the target machine to be driven;

Fig. 12 is a block diagram showing a servo controller in accordance with embodiment 5 of the present invention;

Fig. 13 is a diagram showing an instructed path that is provided for a target machine to be driven by a prior art servo controller, and a response path of the target machine to be driven; and

Fig. 14 is a diagram showing an instructed path that is provided for a target machine to be driven by another prior art servo controller, and a response path of the target machine to be driven.

Embodiment 1.

Fig. 1 is a block diagram showing a servo controller in accordance with embodiment 1 of the present invention. The servo controller 1 shown in the figure drives and controls a machine 2 (i.e., a target machine to be driven) according to a position instruction signal. In the servo controller 1, an FIR (Finite Impulse Response) filter unit 3 makes a correction to the input position instruction signal, a mechanical characteristic compensation unit 4 attenuates components each having a predetermined frequency which corresponds to a characteristic of the machine 2, those components being included in the corrected position instruction signal, and computes a plurality of feed-forward signals respectively associated with the position, speed and torque of the machine 2, and a feedback compensation unit 5 drives the machine 2 according to the plurality of feed-forward signals respectively associated with the position, speed and torque of the machine 2. The FIR filter unit 3 is provided with an FIR filter 6.

In addition, in the mechanical characteristic compensation unit 4, a position instruction computation unit 7 attenuates a component having an antiresonance frequency of the machine 2, which is included in the position instruction signal, so as to compute a feed-forward signal associated with the position of the machine, a differentiator 8 differentiates the position instruction signal, a speed instruction computation unit 9 attenuates a component having the antiresonance frequency of the machine 2, which is included in the differentiated value computed by the differentiator 8, so as to compute a feed-forward signal associated with the speed

of the machine, a computation unit 10 differentiates the differentiated value computed by the differentiator 8 and multiplies the differentiated result by the total inertia of the machine 2, a torque instruction computation unit 11
5 attenuates a component having a resonance frequency of the machine 2, which is included in a value computed by the computation unit 10, so as to compute a feed-forward signal associated with the torque of the machine.

In addition, in the feedback compensation unit 5, a
10 subtractor 12 subtracts a motor position signal from the feed-forward signal associated with the position of the machine and delivers the subtraction result to a position control unit 13, the position control unit 13 acquires a speed control signal from the subtraction result from the subtractor
15 12, an adder/subtractor 14 adds the feed-forward signal associated with the speed of the machine to the speed control signal, subtracts a motor speed signal from the addition result, and delivers the subtraction result to a speed control unit
20 15, the speed control unit 15 acquires a torque control signal from the subtraction result from the adder/subtractor 14, and an adder 16 adds the feed-forward signal associated with the torque of the machine to the torque control signal from the speed control unit 15 and delivers the addition result to the machine 2 as a motor torque instruction signal. The machine
25 2 is provided with a motor 17 for driving a load 18 according to the motor torque instruction signal from the feedback compensation unit 5.

Next, a description will be made as to the operation of the servo controller in accordance with embodiment 1 of the
30 present invention. In Fig. 1, the input position instruction

signal is smoothed by the FIR filter 6 and is then delivered to the mechanical characteristic compensation unit 4. The FIR filter 6 is comprised of two or more moving average filters connected in series, each of them having a time constant of T_f . The time constant of a moving average filter is equivalent to a value that is obtained by multiplying the number of taps of the moving average filter by a sampling period. In addition, the time constant of T_f is computed from requested path accuracy parameters so that a response path satisfies a requested degree of path accuracy by performing predetermined computations. The requested path accuracy parameters can be a corner sag when the target machine is made to pass through a corner (i.e., a distance between the response path and the corner's peak when the target machine approaches the corner's peak most), an amount of inward turning in an arc (i.e., an amount of decrease in the radius of the response path with respect to an instructed radius), and so on.

In the mechanical characteristic compensation unit 4, an input signal x_{r1} applied to the mechanical characteristic compensation unit 4 is applied to the position instruction computation unit 7 first, and the position instruction computation unit 7 then computes a feed-forward signal x_s associated with the position of the machine from the input signal x_{r1} . The position instruction computation unit 7 is a computation unit that attenuates and delivers a component having an antiresonance frequency ω_z of the machine 2, which is included in the input signal x_{r1} . A relationship between the input signal x_{r1} and the output signal x_s is given by the following equation (1), where s is a Laplacian operator.

$$x_a(s) = \left(1 + \frac{1}{\omega_z^2} s^2 \right) x_{r1}(s) \quad (1)$$

The input signal x_{r1} applied to the mechanical characteristic compensation unit 4 is further input to the speed instruction computation unit 9 after differentiated by the differentiator 8, and the speed instruction computation unit 9 then computes a feed-forward signal v_a associated with the speed of the machine from the differentiated input signal v_{r1} . The speed instruction computation unit 9 is a computation unit that attenuates and delivers a component having an antiresonance frequency ω_z of the machine 2, which is included in the differentiated input signal v_{r1} . A relationship between the differentiated input signal v_{r1} and the output signal v_a is given by the following equation (2):

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$$v_a(s) = \left(1 + \frac{1}{\omega_z^2} s^2 \right) v_{r1}(s) \quad (2)$$

In addition, the output signal of the differentiator 8 is input to the torque instruction computation unit 11 after differentiated and then multiplied by the total inertia J of the machine 2 by the computation unit 10, and the torque instruction computation unit 11 then computes a feed-forward signal τ_a associated with the torque of the machine from the output of the computation unit 10. The total inertia J is the

sum of the inertia of the motor 17 and the inertia of the load 18. The torque instruction computation unit 11 is a computation unit that attenuates and delivers a component having a resonance frequency ω_p of the machine 2, which is included in the input signal τ_{r1} applied thereto. A relationship between the input signal τ_{r1} and the output signal τ_a is given by the following equation (3):

$$\tau_a(s) = \left(1 + \frac{1}{\omega_p^2} s^2 \right) \tau_{r1}(s) \quad (3)$$

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Then, the feed-forward signal x_a associated with the position of the machine, the feed-forward signal v_a associated with the speed of the machine, and the feed-forward signal τ_a associated with the torque of the machine are input to the feedback compensation unit 5. In the feedback compensation unit 5, the subtractor 12 subtracts the motor position signal x_m delivered thereto from the machine 2 from the feed-forward signal x_a associated with the position of the machine and delivers the subtraction result to the position control unit 13, and the position control unit 13 determines a speed control signal v_c from the subtraction result from the subtractor 12. Although the position control unit 13 can have any structure as long as the feedback control system becomes stable, a proportional controller or the like is generally used as the position control unit 13. The adder/subtractor 14 then subtracts the motor speed signal v_m delivered thereto from the machine 2 from a value that is obtained by adding the

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feed-forward signal v_a associated with the speed of the machine to the speed control signal v_c from the position control unit 13, and delivers the subtraction result to the speed control unit 15. The speed control unit 15 then determines a torque control signal τ_c from the subtraction result. Although the speed control unit 15 can have any structure as long as the feedback control system becomes stable, a proportional integration controller or the like is generally used as the speed control unit 15. The adder 16 adds the feed-forward signal τ_a associated with the torque of the machine to the torque control signal τ_c from the speed control unit 15 and then delivers the addition result to the machine 2 as the motor torque instruction signal τ_m . As a result, the motor 17 is driven by the motor torque instruction signal. In the machine 2, the motor 17 mounted on a motor mounting base is coupled with the load 18 by way of a torque transmission mechanism, and delivers both the motor position signal x_m and the motor speed signal v_m to the servo controller by using a rotation detector installed in the motor 17. The torque generated by the motor 17 can respond quickly to the motor torque instruction signal τ_m from the servo controller.

In the servo controller having the above-mentioned structure, because according to the vibration characteristics of the machine 2 the feed-forward signals respectively associated with the position, speed, and torque of the machine, which are appropriately computed so that the position of the load of the machine 2 responds completely to the input signal x_{r1} applied to the mechanical characteristic compensation unit 4, are delivered to the feedback compensation unit 5, the load position x_1 responds completely to the input signal x_{r1} applied

to the mechanical characteristic compensation unit 4. This feature can be expressed by the following equation (4) showing a relationship between the motor torque instruction signal τ_m and the motor position x_m when the machine 2 can be approximated as a two-inertia oscillation system.

$$x_m(s) = \frac{1}{Js^2} \frac{1 + \frac{1}{\omega_z^2} s^2}{1 + \frac{1}{\omega_p^2} s^2} \tau_m(s) \quad (4)$$

Furthermore, a relationship between the motor position x_m and the load position x_l is given by the following equation (5):

$$x_l(s) = \frac{1}{1 + \frac{1}{\omega_z^2} s^2} x_m(s) \quad (5)$$

In addition, a relationship between the motor speed v_m and the motor position x_m is given by the following equation (6):

$$v_m(s) = s \cdot x_m(s) \quad (6)$$

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In addition, when the transfer functions of the position control unit 13 and the speed control unit 15 are represented by $C_p(s)$ and $C_v(s)$, respectively, a relationship between the

input and output of the feedback compensation unit 5 is given by the following equation (7):

$$\begin{aligned} \tau_m(s) = & C_v(s) (C_p(s) (x_a(s) - x_m(s)) + v_a(s) - v_m(s)) \\ & + \tau_a(s) \end{aligned} \quad (7)$$

In consideration of the equations (1) to (5) and the relationships shown by the equations (6) and (7), a relationship between the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 and the load position x_1 of the machine 2 in accordance with embodiment 1 is determined as being $x_1 = x_{r1}$. In other words, the load position x_1 responds completely to the input signal x_{r1} applied to the mechanical characteristic compensation unit 4. Therefore, the response characteristics of the machine 2 showing a response of the load position with respect to the instructed position is made to agree with the response characteristics of the FIR filter 6.

Fig. 2 is a diagram showing a symmetric impulse response. When the FIR filter 6 exhibits an impulse response close to that as shown in Fig. 2, it is well known that a symmetric input applied to the FIR filter yields a symmetric output, and therefore a response path with respect to a symmetric instructed path becomes symmetric and go and return response paths have almost the same shape when the load of the machine is made to reciprocatingly move along the same path. In addition, when the FIR filter 6 has a completely symmetric impulse response, that is, when the FIR filter 6 is a linear phase FIR filter, the response path with respect to a symmetric instructed path becomes completely symmetric. Therefore,

when the target to be driven is made to travel between two positions along the same path, the two response paths of the round trip of the target match each other. Furthermore, when the feed-forward signal τ_1 associated with the torque of the machine contains the fourth or lower derivative of the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 and the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 is not smoothed sufficiently, it can be assumed that the feed-forward signal τ_1 associated with the torque of the machine has an impulse, very large value and has a bad influence upon the machine 2. However, because the FIR filter 6 is composed of two or more moving average filters connected in series, when the position instruction signal x_{r1} indicates an acceleration step instruction that is widely used for position control, the fourth derivative of the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 doesn't yield an impulse signal and therefore the feed-forward signal τ_1 associated with the torque of the machine can be prevented from containing an impulse, very large component. Furthermore, because the FIR filter 6 has a completely symmetric impulse response, the response path with respect to a symmetric instructed path becomes completely symmetric, and therefore, when the target to be driven is made to travel between two positions along the same path, the two response paths of the round trip of the target machine match each other.

It is preferable that the FIR filter 6 is a filter having a linear phase characteristic, such as a linear phase FIR filter. As an alternative, the FIR filter 6 can be a general FIR filter that doesn't have a linear phase characteristic. Because the

output of such a general FIR filter is determined from a history of an input applied during a past finite time period, a symmetric response path can be provided easily as compared with the case of using another type of filter other than FIR filters, i.e., an IIR (Infinite Impulse Response) filter. A detailed explanation of FIR filters is made by "Introduction to Filter Circuits", by F. R. Connor (Morikita Suppan), for example. Next, advantages provided by the servo controller according to this embodiment 1 will be explained in simulation. Fig. 3 is a block diagram showing the whole of a system including two servo controllers in accordance with embodiment 1 of the present invention. As shown in the figure, an x-axis servo controller 1a and a y-axis servo controller 1b drive a machine 2 having two degrees of freedom (i.e., two axes of free motion) by using an x-axis motor 17a and a y-axis motor 17b. Fig. 4 is a diagram showing an instructed path that is provided for the target to be driven by the servo controller according to the embodiment 1 of the present invention, and a response path of the target to be driven. In the figure, the instructed path corresponds to the shape of a corner having an angle of 90 degrees, and the response path is provided when the target to be driven is made to move between two positions and in two directions of travel A and B along the same path. In this case, the resonance frequency ω_p of the machine 2 is 300rad/s, and the antiresonance frequency ω_a of the machine 2 is 200rad/s. It should be noted that in the example shown in Fig. 4, vibrations are further reduced in the response path as compared with the prior art case shown by the reference 1, and the difference between the response paths of the round trip is further reduced as compared with the prior art case shown by

the reference 2. As a result, when machining a mold or the like with reciprocating machining, the servo controller system in accordance with embodiment 1 of the present invention can prevent scratches from being made on a machined surface of the
5 mold.

As mentioned above, according to this embodiment 1, when the machine 2 can be assumed to be a two-inertia oscillation system and the attenuation characteristics of the machine 2 due to viscous friction can be neglected, the mechanical
10 characteristic compensation unit 4 can determine feed-forward signals respectively associated with the position, speed, and torque of the machine 2 by using characteristic values of the machine 2 (e.g., the resonance frequency, antiresonance frequency, and total inertia of the machine), thereby reducing
15 vibrations that originate from the characteristics of the machine 2.

Furthermore, by delivering the feed-forward signals acquired by the mechanical characteristic compensation unit 4 to the feedback compensation unit 5, the servo controller
20 makes it possible for the position of the machine 2 to respond completely to the input of the mechanical characteristic compensation unit 4, i.e., the output of the FIR filter unit 3. In addition, because the FIR filter unit 3 can easily make the response path with respect to a symmetric instructed path
25 become symmetric, and, when the target machine is made to travel between two positions along the same path, can make the two response paths of the round trip of the target machine match each other, the servo controller can provide machined surfaces having no irregularities even when carrying out reciprocating
30 machining.

In addition, because the FIR filter unit 3 is constructed of two or more moving average filters connected in series and the time constant of each moving average filter is set according to the requested path accuracy, the symmetry of the response path can be maintained and the signal input to the feedback compensation unit 5 can become an impulse signal having a large amplitude. As a result, it is possible to prevent large shock from being applied to the machine 2 and to make an error of the response path with respect to the instructed path fall within the requested path accuracy.

Embodiment 2.

Fig. 5 is a block diagram showing a servo controller in accordance with embodiment 2 of the present invention. In the figure, a first-order delay filter 21 is disposed in a mechanical characteristic compensation unit 4, and has a time constant that is set according to the damping constant, antiresonance frequency, and load inertia of a machine 2 so that the influence of the attenuation characteristics of the machine 2 due to viscous friction is reduced. The first-order delay filter 21 is so constructed as to correct a position instruction signal filtered by an FIR filter unit 3. A position instruction computation unit 22 then attenuates a component having an antiresonance frequency of the machine 2, which is included in the position instruction signal corrected by the first-order delay filter 21, in consideration of the attenuation characteristics of the machine 2 due to viscous friction so as to compute a feed-forward signal associated with the position of the machine. A speed instruction computation unit 23 attenuates a component having an antiresonance

frequency of the machine 2, which is included in a value computed by a differentiator 8, in consideration of the attenuation characteristic of the machine 2 due to viscous friction so as to compute a feed-forward signal associated with the speed of the machine. A torque instruction computation unit 24 attenuates a component having a resonance frequency of the machine 2, which is included in a value computed by the computation unit 10, in consideration of the attenuation characteristic of the machine 2 due to viscous friction so as to compute a feed-forward signal associated with the torque of the machine. The servo controller in accordance with embodiment 2 of the present invention has the same structure as that of Fig. 1, except that the mechanical characteristic compensation unit 4 includes the first-order delay filter 21 that is so constructed as to correct the position instruction signal filtered by the FIR filter unit 3, as previously mentioned, and each of the position instruction computation unit 22, speed instruction computation unit 23 and torque instruction computation unit 24 of the mechanical characteristic compensation unit 4 is so constructed as to take the attenuation characteristic of the machine 2 due to viscous friction into consideration.

Next, a description will be made as to the operation of the servo controller in accordance with embodiment 2 of the present invention. In Fig. 5, the servo controller in accordance with embodiment 2 of the present invention differs from that according to above-mentioned embodiment 1 in that after correcting the input signal x_{r1} applied to the mechanical characteristic compensation unit 4, the first-order delay filter 21 delivers the input signal x_{r1} to both the position

instruction computation unit 22 and the differentiator 8, and each of the position instruction computation unit 22, speed instruction computation unit 23 and torque instruction computation unit 24 of the mechanical characteristic compensation unit 4 is so constructed as to take the attenuation characteristic of the machine 2 due to viscous friction into consideration. In the servo controller according to above-mentioned embodiment 1, when the influence of the attenuation characteristic of the machine 2 due to the viscous friction of the machine cannot be neglected, there are cases where the influence of the attenuation characteristic of the machine 2 can cause a phase shift between the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 and a load position x_1 , and the load position x_1 cannot be made to properly respond to the input signal x_{r1} applied to the mechanical characteristic compensation unit 4.

The time constant of the first-order delay filter 21 is set so that the phase shift between the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 and the load position x_1 is canceled, the phase shift originating from the attenuation characteristic of the machine 2 due to the viscous friction of the machine. The first-order delay filter 21 makes a correction to the input signal x_{r1} applied to the mechanical characteristic compensation unit 4. A relationship between the input signal x_{r1} and output signal x_{r2} of the first-order delay filter 21 is given by the following equation (8):

$$x_{r2}(s) = \frac{1}{1 + 2\frac{\xi_z}{\omega_z}s} x_{r1}(s) \quad (8)$$

By using the damping constant c , antiresonance frequency ω_z , and load inertia J_1 of the machine 2, ξ_z is given by the following equation (9):

$$\xi_z = \frac{c}{2\omega_z J_1} \quad (9)$$

The position instruction computation unit 22 attenuates a component having an antiresonance frequency ω_z of the machine 2, which is included in the input signal x_{r2} corrected by the first-order delay filter 21, in consideration of the attenuation characteristic of the machine 2, and outputs the attenuated component. A relationship between the input signal x_{r2} and output signal x_a of the position instruction computation unit 22 is given by the following equation (10):

$$x_a(s) = \left(1 + 2\frac{\xi_z}{\omega_z}s + \frac{1}{\omega_z^2}s^2 \right) x_{r2}(s) \quad (10)$$

The speed instruction computation unit 23 attenuates a component having an antiresonance frequency ω_z of the machine 2, which is included in the input signal v_{r1} from the differentiator 8, in consideration of the attenuation

characteristic of the machine 2, and outputs the attenuated component. A relationship between the input signal v_{r1} and output signal v_a of the speed instruction computation unit 23 is given by the following equation (11):

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$$v_a(s) = \left(1 + 2 \frac{\xi_z}{\omega_z} s + \frac{1}{\omega_z^2} s^2 \right) v_{r1}(s) \quad (11)$$

The torque instruction computation unit 24 attenuates a component having a resonance frequency ω_p of the machine 2, which is included in the input signal τ_{r1} , in consideration of the attenuation characteristic of the machine 2, and outputs the attenuated component. A relationship between the input signal τ_{r1} and output signal τ_a of the torque instruction computation unit 24 is given by the following equation (12):

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$$\tau_a(s) = \left(1 + 2 \frac{\xi_p}{\omega_p} s + \frac{1}{\omega_p^2} s^2 \right) \tau_{r1}(s) \quad (12)$$

By using the damping constant c , resonance frequency ω_p , load inertia J_l , and motor inertia J_m of the machine, ξ_z is given by the following equation (13):

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$$\xi_p = \frac{c}{2\omega_p} \left(\frac{1}{J_m} + \frac{1}{J_l} \right) \quad (13)$$

Even when the machine 2 has attenuation characteristics

due to viscous friction or the like, the servo controller constructed as above can make the load position x_l respond completely to the input signal x_{l1} applied to the mechanical characteristic compensation unit 4. This feature can be expressed by the following equation. In other words, when the machine 2 can be approximated as a two-inertia oscillation system and has attenuation characteristics, a relationship between a motor torque instruction signal τ_m and the motor position x_m is given by the following equation (14):

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$$x_m(s) = \frac{1}{Js^2} \frac{1 + 2\frac{\xi_z}{\omega_z}s + \frac{1}{\omega_z^2}s^2}{1 + 2\frac{\xi_p}{\omega_p}s + \frac{1}{\omega_p^2}s^2} \tau_m(s) \quad (14)$$

Furthermore, a relationship between the motor position x_m and the load position x_l is given by the following equation (15):

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$$x_l(s) = \frac{1 + 2\frac{\xi_z}{\omega_z}s}{1 + 2\frac{\xi_z}{\omega_z}s + \frac{1}{\omega_z^2}s^2} x_m(s) \quad (15)$$

Furthermore, a relationship between the motor speed v_m and the motor position x_m and a relationship between an input and an output of a feedback compensation unit 5 are the same as those of the servo controller according to above-mentioned

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embodiment 1, respectively, and are given by the equations (6) and (7), respectively. When the equations (6) and (7), and (8) to (15) are established, a relationship between the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 of the servo controller according to the embodiment 2 and the position x_1 of the load of the machine 2 becomes $x_1 = x_{r1}$. In other words, the load position x_1 responds completely to the input signal x_{r1} applied to the mechanical characteristic compensation unit 4. Therefore, the response characteristics of the machine 2 showing a response of the load position with respect to the instructed position is made to agree with the response characteristics of the FIR filter 6, and a response path that is symmetric and excites no vibrations can be acquired.

Next, advantages provided by the servo controller according to this embodiment 2 will be explained based on results in simulation. Fig. 6A is a diagram showing an instructed path that is provided for the target machine to be driven by the servo controller in accordance with embodiment 2 of the present invention, and a response path of the target machine to be driven. Fig. 6A shows an instructed path and a response path of the machine 2 that is driven by the servo controller according to this embodiment 2, the machine having two degrees of freedom, i.e., two axes (x and y axes) of free motion, and Fig. 6B shows an instructed path that is provided for the machine 2 to be driven by the servo controller according to above-mentioned embodiment 1 and a response path of the machine. In these figures, the instructed path corresponds to the shape of a corner having an angle of 90 degrees, and it is assumed that the resonance frequency ω_p of the machine

2 is 300rad/s, and the antiresonance frequency ω_z of the machine 2 is 200rad/s. In addition, it is assumed that the attenuation ratio ζ_p of the machine 2 is 0.2. As can be seen from the example as shown in Figs. 6A and 6B, when the machine 2 has attenuation characteristics, the servo controller according to this embodiment 2 can further reduce vibrations in the response path, as compared with the case of using the servo controller according to above-mentioned embodiment 1.

As mentioned above, according to this embodiment 2, each of the position instruction computation unit 22, speed instruction computation unit 23, and torque instruction computation unit 24 of the mechanical characteristic compensation unit 4 attenuates a component having an antiresonance or resonance frequency of the machine 2 in consideration of the attenuation characteristics of the machine 2 due to the viscous friction of the machine, and the first-order delay filter 21 has a time constant that is set so that the phase shift between the input signal x_{r1} applied to the mechanical characteristic compensation unit 4 and the load position x_1 is canceled, the phase shift originating from the attenuation characteristic of the machine 2 due to the viscous friction of the machine, and is so constructed as to make a correction to the input signal x_{r1} applied to the mechanical characteristic compensation unit 4. Therefore, even when the machine 2 can be assumed to be a two-inertia oscillation system and the machine 2 has attenuation characteristics due to the viscous friction thereof, the servo controller in accordance with embodiment 2 of the present invention can make the machine position, i.e., the load position completely respond to the input of the mechanical

characteristic compensation unit 4, i.e., the output of the FIR filter unit 3 without exciting mechanical vibrations.

Embodiment 3.

5 Fig. 7 is a block diagram showing a servo controller in accordance with embodiment 3 of the present invention. As shown in the figure, a fifth-order IIR filter (or an nth-order filter) 31 is disposed in a mechanical characteristic compensation unit 4. The fifth-order IIR filter has a property
10 of cutting off desired frequencies and corrects a position instruction signal passing through an FIR filter unit. The servo controller in accordance with embodiment 3 of the present invention has the same structure as that of Fig. 1, except that the mechanical characteristic compensation unit 4 includes the
15 fifth-order filter 31 that is so constructed as to correct the position instruction signal filtered by the FIR filter unit 3.

Next, a description will be made as to the operation of the servo controller in accordance with embodiment 3 of the
20 present invention. In Fig. 7, the servo controller in accordance with embodiment 3 of the present invention differs from that according to above-mentioned embodiment 1 in that after correcting the input signal x_n applied to the mechanical characteristic compensation unit 4 by using the fifth-order
25 IIR filter 31, the mechanical characteristic compensation unit 4 delivers the corrected input signal to both a position instruction computation unit 7 and a differentiator 8. It can be assumed that the fifth-order IIR filter 31 has a structure shown by the following equation (16):

$$x_{r2}(s) = \frac{1}{\left(1 + \frac{1}{K_1}s\right)\left(1 + \frac{1}{K_2}s\right)\left(1 + \frac{1}{K_3}s\right)\left(1 + \frac{1}{K_4}s\right)\left(1 + \frac{1}{K_5}s\right)} x_{r1}(s) \quad (16)$$

where K_1 to K_5 are parameters showing poles that determine the frequency cutoff characteristics of the fifth-order IIR filter

5. 31.

Fig. 8 is a diagram showing an example of a gain curve of the fifth-order IIR filter. The example of Fig. 8 shows the gain curve of the fifth-order IIR filter 31 at $K_1 = K_2 = K_3 = K_4 = K_5 = 1000$. It is apparent from this figure that
10 components of frequencies higher than about 400rad/s are cut off by the fifth-order IIR filter.

According to the servo controller having such a structure, even when the machine 2 cannot be approximated as a two-inertia oscillation system and another resonance point exists in a
15 frequency region that is higher than the resonance frequency ω_p of the machine, because components of frequencies that are close to the other resonance point are cut off by the fifth-order IIR filter 31, vibrations in the response path can be reduced. Furthermore, even when the position instruction
20 signal contains noise of high frequency and hence vibrations are caused in the response path, because components of high frequencies included in the position instruction signal are cut off by the fifth-order IIR filter 31, vibrations in the response path can be reduced.

25 Next, advantages provided by the servo controller according to this embodiment 3 will be explained based on

results in simulation. Fig. 9A is a diagram showing an instructed path that is provided for the target machine to be driven by the servo controller in accordance with embodiment 3 of the present invention, and a response path of the target machine to be driven. Fig. 9A shows an instructed path and a response path of the machine 2 that is driven by the servo controller according to this embodiment 3, the machine having two degrees of freedom, i.e., two axes (x and y axes) of free motion, and Fig. 9B shows an instructed path that is provided for the machine 2 to be driven by the servo controller according to above-mentioned embodiment 1 and a response path of the machine. In these figures, the instructed path corresponds to the shape of a corner having an angle of 90 degrees, and it is assumed that the resonance frequency ω_p of the machine 2 is 300rad/s, and the antiresonance frequency ω_z of the machine 2 is 200rad/s. In addition, it is assumed that the machine 2 has a second resonance frequency of 1000rad/s, and a second antiresonance frequency of 700rad/s. As can be seen from the example as shown in Figs. 9A and 9B, when the machine 2 cannot be approximated as a two-inertia oscillation system and has both a second resonance frequency and a second antiresonance frequency, the servo controller according to this embodiment 3 can further reduce vibrations in the response path, as compared with the case of using the servo controller according to above-mentioned embodiment 1.

As mentioned above, according to this embodiment 3, because the mechanical characteristic compensation unit 4 is provided with the fifth-order IIR filter 31 that has a property of cutting off desired frequencies and corrects the input position instruction signal, when noise of high frequency is

included in the position instruction signal and when another resonance point and another antiresonance point exist in a frequency region that is higher than the resonance frequency and antiresonance frequency of the machine 2, which are
5 parameters of the mechanical characteristic compensation unit 4, the bad influence upon the response path can be reduced. In accordance with this embodiment 3, the fifth-order IIR filter 31 having five desired poles is disposed in the mechanical characteristic compensation unit 4. As an
10 alternative, a first or higher-order IIR filter can be disposed in the mechanical characteristic compensation unit 4.

Embodiment 4.

Fig. 10 is a block diagram showing a servo controller
15 in accordance with embodiment 4 of the present invention. In the figure, the servo controller delivers a position instruction signal directly applied to a mechanical characteristic compensation unit 4 to a subtractor 12 as a feed-forward signal associated with the position of a machine
20 2, a differentiator 8 differentiates the input position instruction signal so as to compute a feed-forward signal associated with the speed of the machine 2 and then delivers it to an adder/subtractor 14, a computation unit 10 further differentiates the differentiated position instruction signal
25 computed by the differentiator 8 and multiplies the differentiated result by a total inertia of the machine 2, and a vibration reduction filter 41 attenuates a component having a resonance frequency of the machine 2 included in the value computed by the computation unit 10 and amplifies a component
30 having an antiresonance frequency of the machine 2 included

in the value computed by the computation unit 10 so as to compute a feed-forward signal associated with the torque of the machine 2, and delivers it to an adder 16. The servo controller in accordance with embodiment 4 of the present invention has the same structure as that of Fig. 1, except that the mechanical characteristic compensation unit 4 is constructed as above.

Next, a description will be made as to the operation of the servo controller in accordance with embodiment 4 of the present invention. In Fig. 10, the position instruction signal x_r directly applied to the mechanical characteristic compensation unit 4 is delivered to a feedback compensation unit 5 as the feed-forward signal x_a associated with the position of the machine. Furthermore, the position instruction signal is differentiated by the differentiator 8 and is then delivered to the feedback compensation unit 5 as the feed-forward signal v_a associated with the speed of the machine. In addition, after the differentiated signal computed by the differentiator 8 is further differentiated by the computation unit 10 and is then multiplied by the total inertia of the machine 2, the multiplication result is delivered to the vibration reduction filter 41, and the output signal of the vibration reduction filter 41 is delivered to the feedback control unit 5 as the feed-forward signal τ_a associated with the torque of the machine. The structures and operations of the feedback compensation unit 5 and the machine 2 are the same to those according to above-mentioned embodiment 1.

Next, the operation of the vibration reduction filter 41 will be explained. It is assumed that a relationship between the input signal τ_{r1} applied to the vibration reduction

filter 41 and the output signal τ_a of the vibration reduction filter 41 is given by the following equation (17) by using the resonance frequency ω_p and antiresonance frequency ω_z of the machine 2.

5

$$\tau_a(s) = \frac{1 + \frac{1}{\omega_p^2} s^2}{1 + \frac{1}{\omega_z^2} s^2} \tau_{r1}(s) \quad (17)$$

The vibration reduction filter 41 thus attenuates the component having the resonance frequency of the machine 2, which is included in the value computed by the computation unit 10, and amplifies the component having the antiresonance frequency of the machine 2, which is included in the value computed by the computation unit 10.

The servo controller according to this embodiment having such a simple structure can reduce mechanical vibrations. Furthermore, when the machine 2 has high stiffness between a motor 17 and a load 18 thereof and low stiffness between the motor 17 and a motor mounting base on which the motor is mounted, and mechanical vibrations occur because of resonance and antiresonance that occur between the motor 17 and the motor mounting base, vibrating components that originate from the resonance and antiresonance that occur between the motor 17 and the motor mounting base are removed by the vibration reduction filter 41 and the load position x_1 completely responds to the position instruction signal x_r . This feature can be expressed by the following equation. In other words, when the machine 2 can be approximated as a model having

sufficiently-high stiffness between the motor 17 and the load 18 and low stiffness between the motor 17 and the motor mounting base, a relationship between a motor torque instruction signal τ_m and a motor position x_m is given by the following equation
 5 (18):

$$x_m(s) = \frac{1}{Js^2} \frac{1 + \frac{1}{\omega_z^2} s^2}{1 + \frac{1}{\omega_p^2} s^2} \tau_m(s) \quad (18)$$

Furthermore, a relationship between the motor position
 10 x_m and a load position x_l is given by the following equation
 (19):

$$x_l(s) = x_m(s) \quad (19)$$

15 Furthermore, a relationship between a motor speed v_m and the motor position x_m and a relationship between the input and output of the feedback compensation unit 5 are the same as those of the servo controller according to above-mentioned embodiment 1, and are given by the equations (6) and (7),
 20 respectively. When the equations (6) and (7), and (17) to (19) are established, a relationship between the input position instruction signal x_r , applied to the mechanical characteristic compensation unit 4 of the servo controller according to the embodiment 4 and the position x_l of the load of the machine
 25 becomes $x_l = x_r$. In other words, the load position x_l responds completely to the input position instruction signal x_r .

Therefore, mechanical vibrations can be effectively reduced.

Next, advantages provided by the servo controller according to this embodiment 4 will be explained based on results in simulation. Fig. 11 is a diagram showing an instructed path that is provided for the target machine to be driven by the servo controller in accordance with embodiment 4 of the present invention, and a response path of the target machine to be driven. Fig. 11 shows an instructed path and a response path of the machine 2 that is driven by the servo controller according to this embodiment 4, the machine having two degrees of freedom, i.e., two axes (x and y axes) of free motion. In the figure, the instructed path corresponds to the shape of a corner having an angle of 90 degrees, and the response path is provided when the target to be driven is made to move between two positions and in two directions of travel A and B along the same path. Furthermore, it is assumed that the machine 2 has sufficiently-high stiffness between the motor 17 and the load 18 thereof and low stiffness between the motor 17 and the motor mounting base on which the motor is mounted, and that the resonance frequency ω_p of the machine 2 is 300rad/s and the antiresonance frequency ω_z of the machine 2 is 200rad/s. As can be seen from the example as shown in Fig. 11, even when the machine 2 has low stiffness between the motor 17 and the motor mounting base thereof, the servo controller according to this embodiment 4 can further reduce vibrations in the response path and the difference between the two response paths of the round trip, as compared with the case of using prior art servo controllers.

As mentioned above, according to this embodiment 4, because the vibration reduction filter 41 attenuates the

component having the resonance frequency of the machine 2, which is included in the value computed by the computation unit 10, and amplifies the component having the antiresonance frequency of the machine 2, which is included in the value
5 computed by the computation unit 10, so as to compute the feed-forward signal associated with the torque of the machine, the servo controller can produce the effect of reducing vibrations with a simpler structure than that of the servo controller according to above-mentioned embodiment 1.
10 Particularly, when vibrations occur because of low stiffness between the motor 17 and the motor mounting base of the machine 2, vibrations in the machine 2 can be reduced.

Embodiment 5.

15 Fig. 12 is a block diagram showing a servo controller in accordance with embodiment 5 of the present invention. In the figure, a position instruction correction unit 51 is disposed between an FIR filter unit 3 and a mechanical characteristic compensation unit 4. The position instruction
20 correction unit 51 has a property of reducing the influence of an FIR filter 6 and a fifth-order IIR filter 31 upon decrease in their gains in a range of frequencies lower than the cutoff frequencies of these filters, and corrects a position instruction signal passing through the FIR filter 6.

25 A simulated position control loop unit 52 performs a simulation of a feedback compensation unit 5 based on both a feed-forward signal associated with the position of a machine and a feed-forward signal associated with the speed of the machine so as to compute a simulated speed signal. A torque
30 correction signal computation unit 53 computes a torque

correction signal according to a change in the sign of the simulated speed signal, and then delivers the torque correction signal to an adder 16 of the feedback compensation unit 5. In the simulated position control loop unit 52, a
5 subtractor 54 subtracts a simulated position signal from the feed-forward signal associated with the position of the machine and then delivers the subtraction result to a second position control unit 55, the second position control unit 55 performs the same computation as done by a position control
10 unit 13, which is explained in embodiment 1, and then delivers the computation result to an adder 56, the adder 56 adds the output of the second position control unit 55 to the feed-forward signal associated with the speed of the machine so as to obtain the simulated speed signal, and an integrator
15 57 integrates the simulated speed signal so as to obtain the simulated position signal. The servo controller in accordance with embodiment 5 of the present invention has the same structure as that of Fig. 7, except that the servo controller further includes the position instruction correction unit 51,
20 the simulated position control loop unit 52, and the torque correction signal computation unit 53.

Next, a description will be made as to the operation of the servo controller in accordance with embodiment 5 of the present invention. As shown in Fig. 12, the servo controller
25 in accordance with embodiment 5 of the present invention differs from that according to above-mentioned embodiment 3 in that after correcting the output signal of the FIR filter unit 3, the position instruction correction unit 51 delivers it to the mechanical characteristic compensation unit 4, the
30 simulated position control loop unit 52 obtains the simulated

speed signal from both the feed-forward signal associated with the position of machine and the feed-forward signal associated with the speed of the machine, which are delivered thereto from the mechanical characteristic compensation unit 4, and the torque correction signal computation unit 53 computes the torque correction signal from the simulated speed signal delivered thereto and then delivers it to the adder 16 so as to cause the adder 16 to add the torque correction signal to the motor torque instruction signal.

The FIR filter 6 and the fifth-order IIR filter 31 smooth the input position instruction signal so as to prevent the signals input to the feedback compensation unit 5 from becoming large impulses, thereby preventing a bad influence from being exerted upon the machine 2. Those filters can also reduce vibrations in the response path by cutting off components having high frequencies included in the position instruction signal. However, because those filters are both low pass filters, their gains decrease as the frequency of the input increases. The gains of those filters can also decrease a little even in a low frequency region of frequencies lower than the cutoff frequency, and this results in the radius of the response path becoming smaller than the radius of the instructed path when the instructed path includes an arc. Therefore, the position instruction correction unit 51 corrects the input position instruction signal so that the influence of the FIR filter 6 and the fifth-order IIR filter 31 upon decrease in their gains is reduced. A relationship between the input signal x_{ri} applied to the position instruction correction unit 51 and an output signal x_{r11} from the position instruction correction unit 51 is given by the following

equation (20):

$$x_{r11}(s) = (1 + \alpha \cdot s) x_{r1} \quad (20)$$

5 where α is a parameter used for increasing or decreasing the amount of correction and is set so that the decrease in the gains in the low frequency range from the frequency of the position instruction signal x_r to the frequency of the output x_{r2} of the fifth-order IIR filter 31 becomes below a desired
10 value.

Furthermore, in a case where a friction force is exerted on the motor 17, when the direction of rotation of the motor 17 is reversed, a time delay can occur in the tracking of the output of the FIR filter unit 3 by the position of the machine
15 2 and this results in the occurrence of a difference between the instructed path and the response path. In this case, by providing a correction instruction for correcting the torque instruction signal when the sign of the motor speed changes, a time delay can be prevented from occurring in the tracking
20 of the output of the FIR filter unit 3 by the position of the machine 2. However, in accordance with the method of providing the correction instruction when the sign of the motor speed signal changes, even when the sign of the motor speed signal changes due to small turbulence applied to the motor 17 or the
25 load 18 while the motor 17 is stopped, the direction of rotation of the motor 17 can be assumed to be reversed and therefore the correction instruction is undesirably provided.

In contrast, the simulated position control loop unit 52 performs a simulation of the feedback compensation unit 5
30 based on both the feed-forward signal associated with the

position of the machine and the feed-forward signal associated with the speed of the machine so as to compute a simulated speed signal, and then delivers it to the torque correction signal computation unit 53. In the simulated position control loop unit 52, the subtractor 54 subtracts the simulated position signal from the feed-forward signal associated with the position of the machine and delivers the subtraction result to the second position control unit 55. The second position control unit 55 performs the same computation as done by the position control unit 13, which is explained in embodiment 1, and then delivers the computation result to the adder 56, the adder 56 adds the output of the second position control unit 55 to the feed-forward signal associated with the speed of the machine so as to obtain the simulated speed signal, and the integrator 57 integrates the simulated speed signal so as to obtain the simulated position signal. The torque correction signal computation unit 53 computes the torque correction signal according to a change in the sign of the simulated speed signal, and then delivers it to the adder 16. The torque correction signal has a value that is predetermined according to a change in the torque of the motor 17 when the direction of rotation of the motor 17 is reversed, which is measured in advance.

As mentioned above, according to this embodiment 5, because the decrease in the gains in a low frequency range of the FIR filter 6 and the fifth-order IIR filter 31 caused by themselves is compensated for by the position instruction correction unit 51, when the instructed path contains an arc, the radius of the response path never becomes smaller than the radius of the instructed path and the difference between the

instructed path and the response path can be reduced. Furthermore, because the simulated position control loop unit 52 computes the simulated speed signal from both the feed-forward signal associated with the position of the machine and the feed-forward signal associated with the speed of the machine and the torque correction signal computation unit 53 computes the torque correction signal according to a change in the sign of the simulated speed signal and then adds the torque correction signal to the motor torque instruction signal, a time delay can be prevented from occurring in the tracking of the output of the FIR filter unit 3 by the position of the machine 2 and the difference between the instructed path and the response path can be reduced.

In accordance with this embodiment 5, the servo controller is further provided with the position instruction correction unit 51, the simulated position control loop unit 52, and the torque correction signal computation unit 53 in addition to the structure of the servo controller according to embodiment 3, as previously explained. As an alternative, the servo controller can be further provided with only the position instruction correction unit 51 or only the simulated position control loop unit 52 and the torque correction signal computation unit 53 of the above-mentioned additional components.

In addition, in accordance with this embodiment 5, the position instruction correction unit 51 is disposed between the FIR filter unit 3 and the mechanical characteristic compensating unit 4, as previously explained. As an alternative, the position instruction correction unit 51 can be disposed at the front of the FIR filter unit 3 or at the

rear of the mechanical characteristic compensating unit 4.

Furthermore, in accordance with this embodiment 5, the servo controller adds the torque correction signal to the motor torque instruction signal, as previously explained. As an alternative, the servo controller can add the torque correction signal to the feed-forward signal associated with the torque of the machine. In this case, when the speed control unit 15 is a controller that carries out proportion and integration control, the servo controller can alternatively add the torque correction signal to an integrated item obtained by the speed control unit 15.

In addition, in accordance with any one of the above-mentioned embodiments, the feedback compensation unit 5 receives the plurality of feed-forward signals respectively associated with the position, speed, and torque of the machine, as previously explained. As an alternative, the feedback compensation unit 5 can receive a feed-forward signal associated with the acceleration of the machine, instead of the feed-forward signal associated with the torque of the machine. In this case, the computation unit 10 according to any one of above-mentioned embodiments can be replaced by a computation unit that only differentiates the differentiated result obtained by the differentiator 8. This variant can provide the same advantage. As an alternative, the feedback compensation unit 5 can receive a feed-forward signal associated with an electric current flowing in the machine, instead of the feed-forward signal associated with the torque of the machine. In this case, the computation unit 10 according to any one of above-mentioned embodiments can be replaced by a computation unit that multiplies the

differentiated result obtained by the differentiator 8 by a value that is obtained by dividing the total inertia of the machine 2 by the torque constant of the motor 17, instead of the total inertia of the machine 2. This variant can provide
5 the same advantage.

Furthermore, in accordance with any one of the above-mentioned embodiments, the motor 17 is of rotation type to generate a torque, as previously explained. As an alternative, the motor 17 can be of linear type to generate
10 thrust. In this case, in any one of above-mentioned embodiments, inertia can be replaced by mass and torque can be replaced by thrust. This variant can provide the same advantage.

As previously explained, the servo controller in
15 accordance with the present invention is applied to the position control of the target machine. As an alternative, the servo controller in accordance with the present invention can be applied to the speed control of the target machine. When the servo controller in accordance with the present invention
20 is applied to the speed control of the target machine, there is no necessity to provide the feedback loop associated with the position of the target machine and the feed-forward signal associated with the position of the target machine. This variant can provide the same advantage.

25 In addition, in accordance with any one of the above-mentioned embodiments, the position instruction operation unit, the speed instruction operation unit, and the torque instruction operation unit can multiply the plurality of feed-forward signals respectively associated with the
30 position, speed, torque of the target machine by either a dead

time caused by discreting or an adjustment factor used for making an adjustment for a slight model error of the target to be controlled, respectively. As an alternative, the differentiator 8 and the computation unit 10 can multiply their
5 respective computed values by a similar adjustment factor.

Furthermore, in accordance with any one of the above-mentioned embodiments, the components of the mechanical characteristic compensating unit 4 are arranged in different order as long as the mechanical characteristic compensating
10 unit 4 has the same transfer function from its input to its output. For example, the feed-forward signal v_s associated with the speed of the target machine can be determined by differentiating the feed-forward signal x_s associated with the position of the target machine. In addition, in any one of
15 the above-mentioned embodiments, differentiation can be replaced by pseudo-differentiation (multiplying the difference between the immediately-preceding value and the current value by a reciprocal of the sampling period so as to compute an approximate derivative).

20 In addition, in accordance with any one of the above-mentioned embodiments 1 to 3, the FIR filter unit 3 and the mechanical characteristic compensating unit 4 can change places. In other words, the position instruction signal is directly applied to the mechanical characteristic
25 compensating unit 4 and the outputs of the mechanical characteristic compensating unit 4 are then input to the FIR filter unit 3. The FIR filter unit 3 finally generates the plurality of feed-forward signals respectively associated with the position, speed, and torque of the target machine from
30 the outputs of the mechanical characteristic compensating unit

4.

Many widely different embodiments of the present invention may be constructed without departing from the spirit and scope of the present invention. It should be understood
5 that the present invention is not limited to the specific embodiments described in the specification, except as defined in the appended claims.